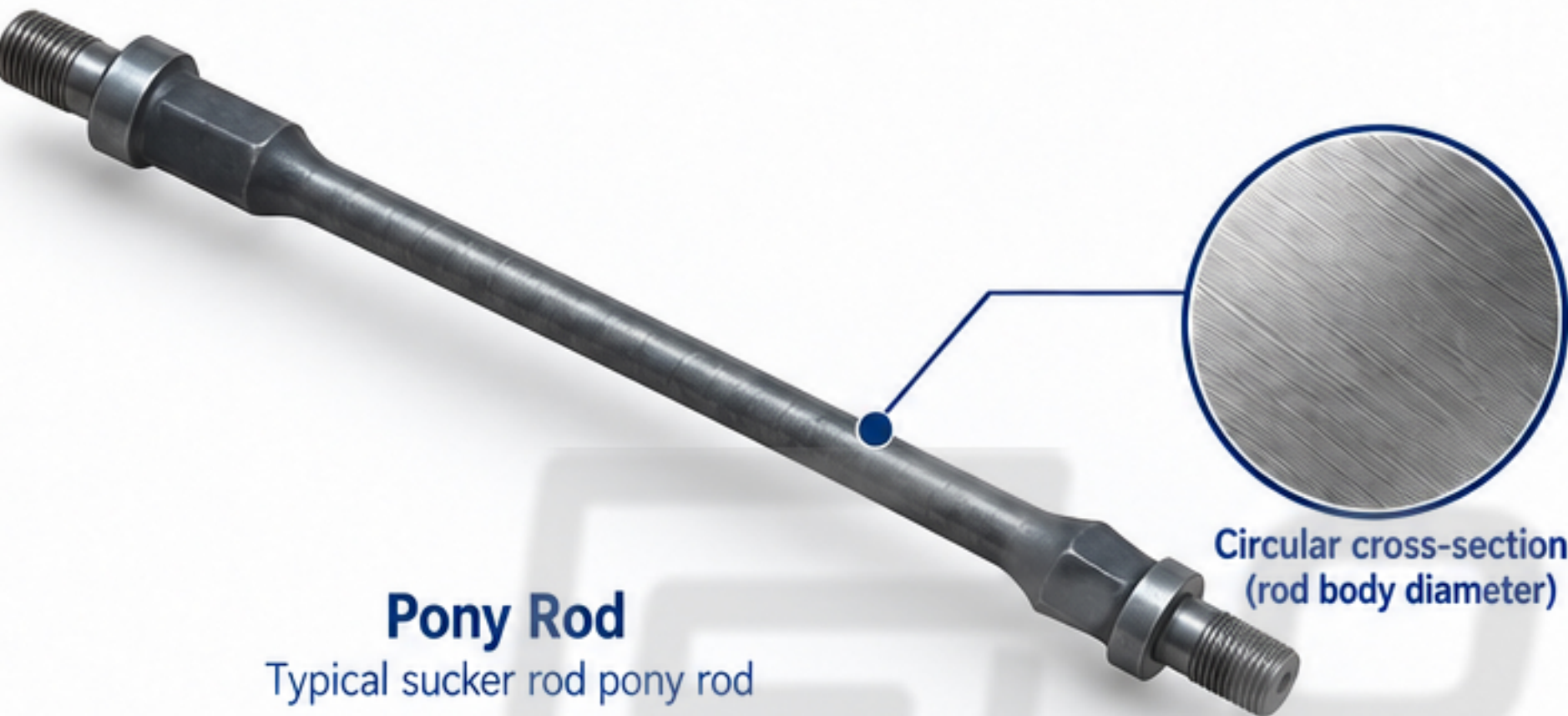


Pony Rod Load, Stress and Fatigue Evaluation Guide

Engineering reference for how rod diameter changes nominal load-bearing area in sucker rod systems.



Pony Rod
Typical sucker rod pony rod

PONY ROD SIZES AND CROSS-SECTIONS

LARGER DIAMETER → LARGER LOAD-BEARING AREA

3/4 in.
(19.05 mm)



285.0 mm²

7/8 in.
(22.23 mm)



388.1 mm²

1 in.
(25.40 mm)



506.7 mm²

CROSS-SECTIONAL AREA

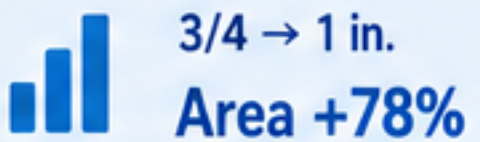
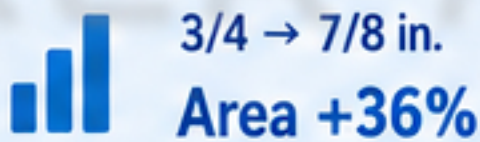
$$A = \frac{\pi d^2}{4}$$

Nominal area based on circular rod-body diameter.

NOMINAL CROSS-SECTIONAL AREA DATA

Pony Rod Size	Body Diameter	Nominal Cross-Sectional Area
3/4 in.	19.05 mm	285.0 mm²
7/8 in.	22.23 mm	388.1 mm²
1 in.	25.40 mm	506.7 mm²

INCREASE IN LOAD-BEARING AREA



ENGINEERING LOGIC

Rod Diameter ↑

Load-Bearing Area ↑

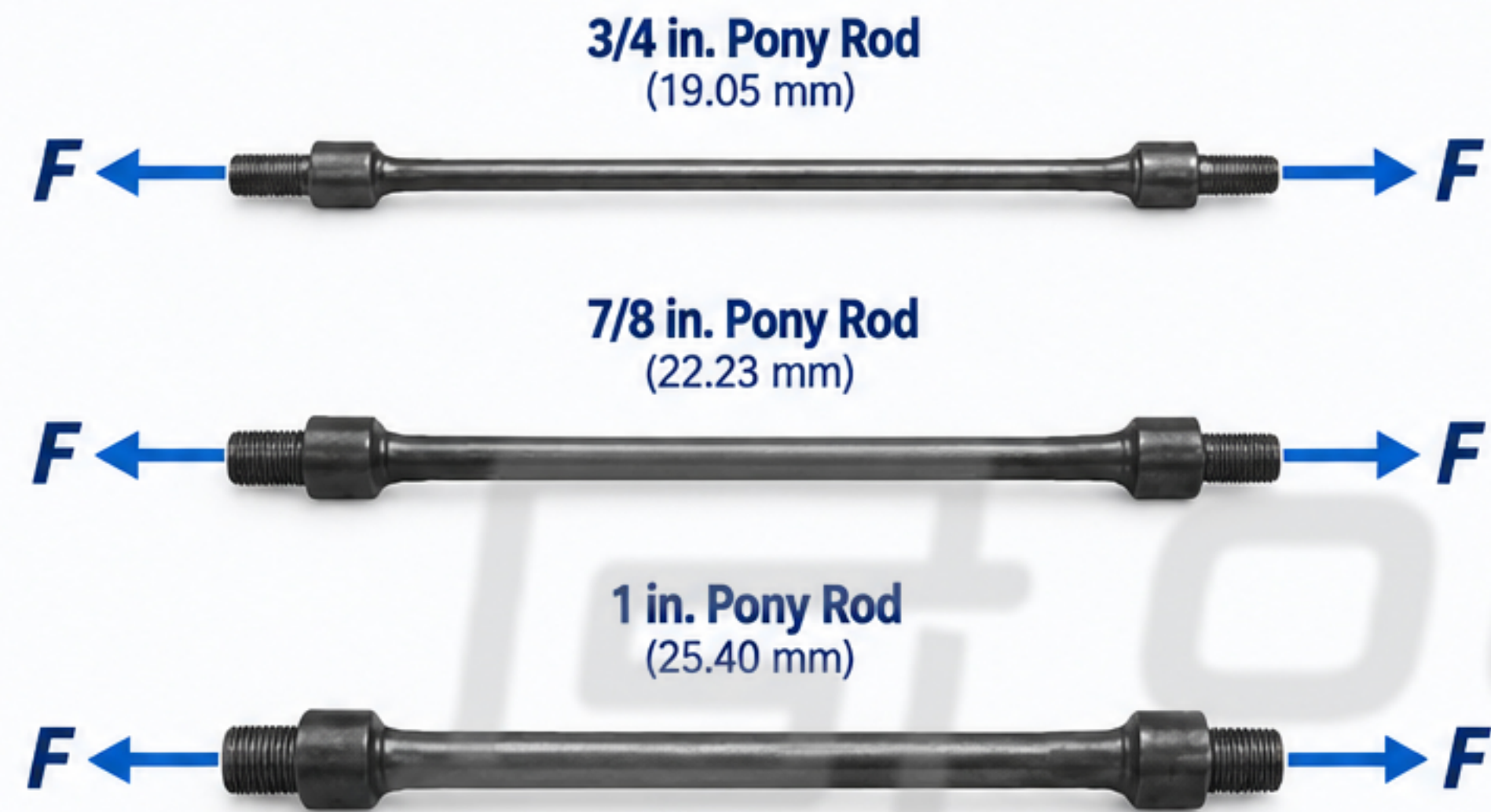
Nominal Axial Stress ↓

Under the same axial load, a larger rod body carries lower nominal stress.

NOTE

Calculated areas are based on nominal circular rod-body diameter and do not include local geometric effects at the upset transition or threaded connection.

SAME AXIAL LOAD — DIFFERENT ROD DIAMETER



$$\sigma = \frac{F}{A}$$

Where:

- σ = nominal axial stress
- F = axial tensile load
- A = nominal rod-body cross-sectional area

Same Load → Different Rod Diameter → Different Nominal Stress

Illustrative Engineering Calculation — Not a Design Load

Axial Load	3/4 in. Pony Rod	7/8 in. Pony Rod	1 in. Pony Rod
20 kN	70.2 MPa	51.5 MPa	39.5 MPa
40 kN	140.3 MPa	103.1 MPa	78.9 MPa
60 kN	210.5 MPa	154.6 MPa	118.4 MPa
80 kN	280.7 MPa	206.1 MPa	157.9 MPa

Stress Comparison at 60 kN

3/4 in.	7/8 in.	1 in.
210.5 MPa	154.6 MPa	118.4 MPa

Larger rod diameter reduces nominal body stress under the same axial load.

Grade Strength Reference

Grade C / K Minimum Yield: 414 MPa

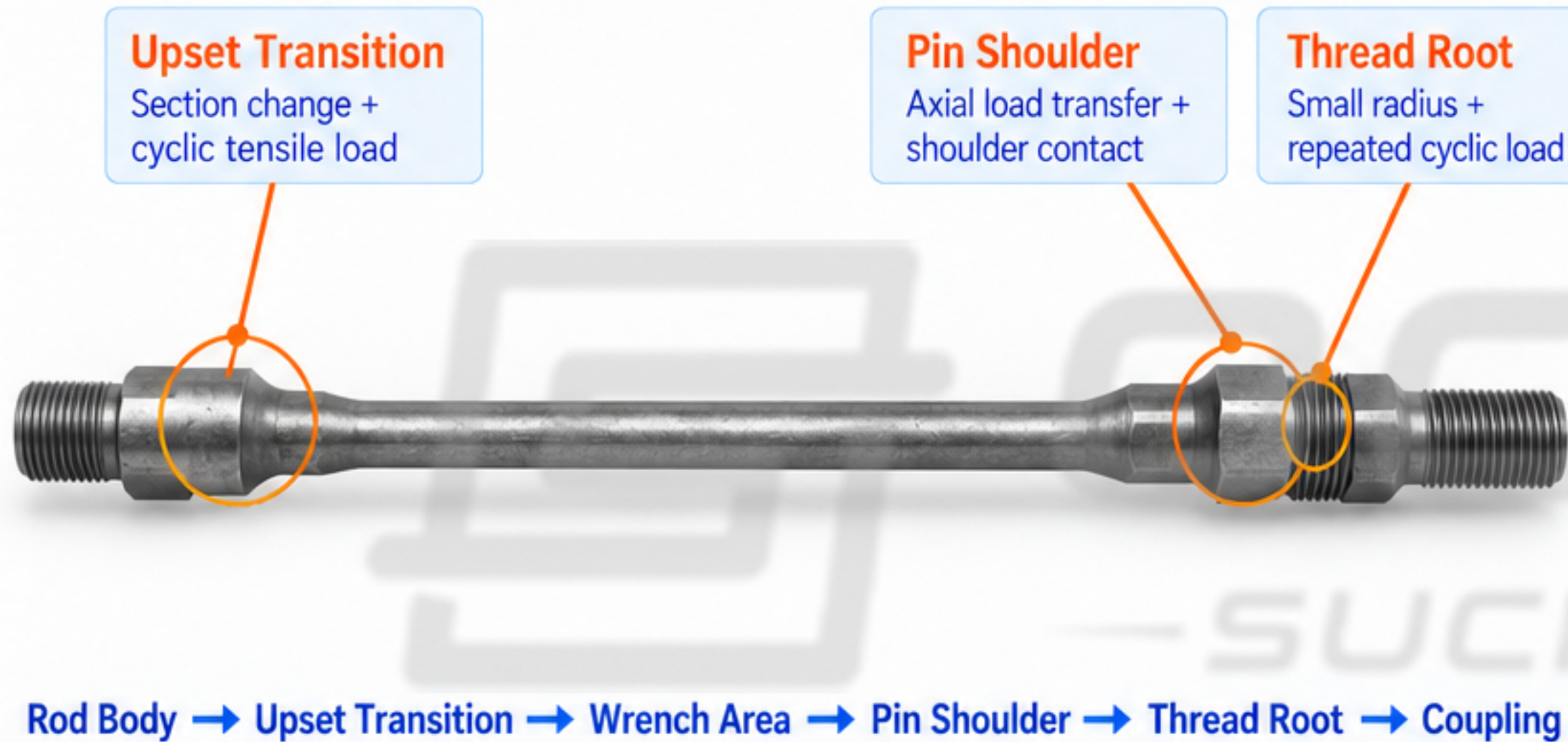
D-Family Minimum Yield: 586 MPa

Nominal body stress is only one part of rod evaluation. Actual cyclic loading, stress concentration, corrosion and connection geometry must also be considered.

KEY TAKEAWAY

Nominal axial stress decreases as rod diameter increases under the same applied load.

FATIGUE-SENSITIVE AREAS IN A PONY ROD

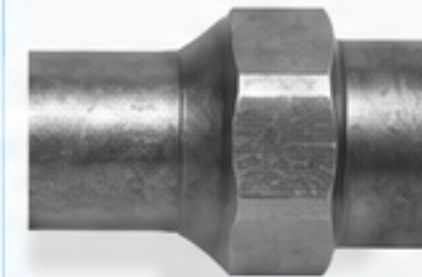


1. Upset Transition



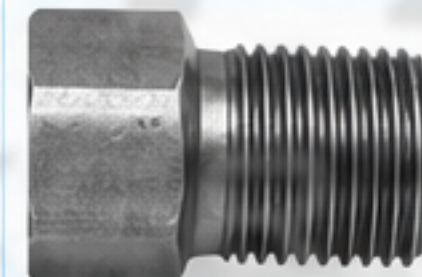
The transition from the rod body to the forged end creates a geometric change in the load path. Poor transition geometry or surface discontinuities can increase local stress concentration.

2. Pin Shoulder



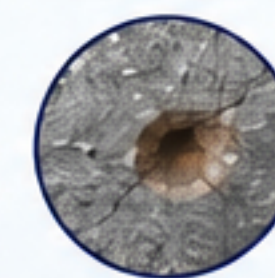
The shoulder forms part of the connection load path and is repeatedly loaded during each pumping cycle. Surface damage or poor geometry can increase local stress.

3. Thread Root

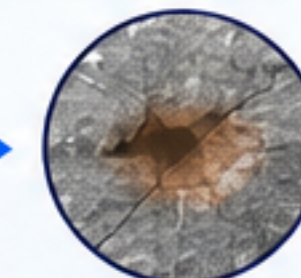


Thread roots naturally create localized stress concentration. Connection damage, corrosion or poor machining can further reduce fatigue resistance.

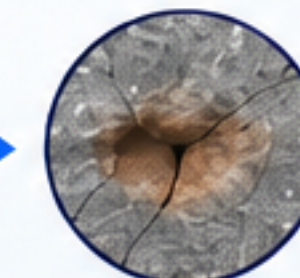
Corrosion-Fatigue Initiation



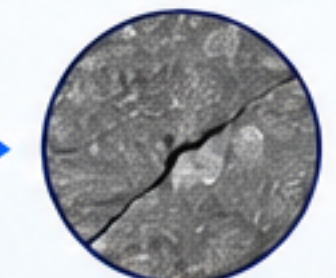
Corrosion Pit



Local Stress Concentration



Crack Initiation



Fatigue Propagation

Corrosion pits can act as fatigue initiation sites under repeated tensile loading.

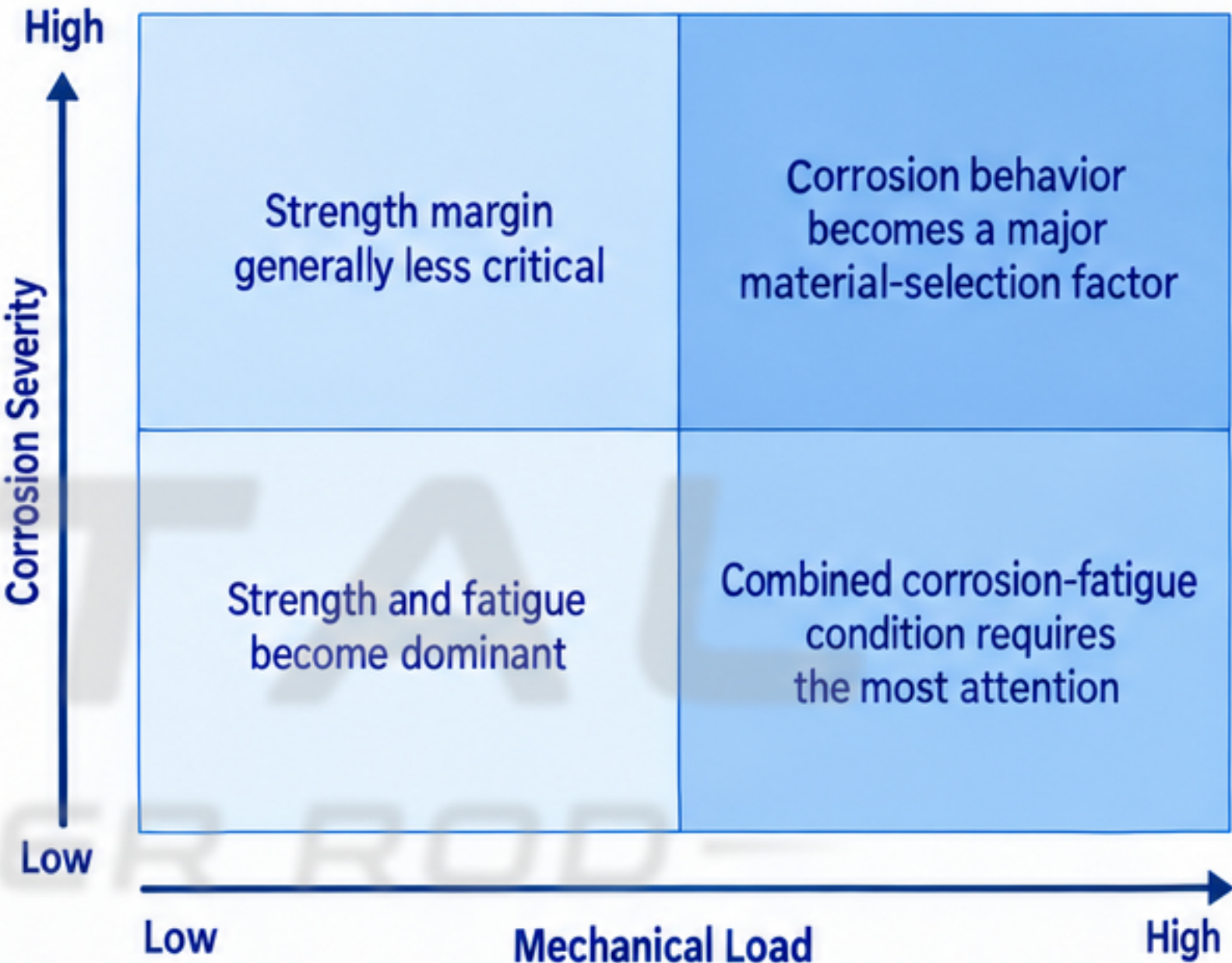
KEY TAKEAWAY

Fatigue risk is governed by local stress concentration and cyclic loading, not by nominal rod-body stress alone.

LOAD AND FATIGUE EVALUATION LOGIC



RISK MATRIX



EVALUATION NOTE



Evaluation should integrate loading, material strength, fatigue-sensitive geometry and corrosion exposure rather than relying on grade designation alone.

KEY TAKEAWAY

Final pony rod evaluation combines axial load, material strength range, local fatigue factors and service environment.